

Determination and evaluation of minimum miscibility pressure using various methods: experimental, visual observation, and simulation

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Abstract. This research proposes a simultaneous technique using various methods to yield the most reliable Minimum Miscibility Pressure (MMP) value. Several methods have been utilized in this study including slim tube test, swelling test, vanishing interfacial tension test, visual observation during swelling test and vanishing interfacial tension test, and simulation. The proposed method may reduce the uncertainty and avoid doubtful MMP. The method can also demonstrate discrepancies among the results. There were two samples used in this study namely Crude Oil AB-5 and Crude Oil AB-4. It showed that for Crude Oil AB-5 the discrepancies among the results from that of the slim tube test were between 3.9% and 10.4% and 0% and 5.9% for the temperature of 60 °C and 66 °C, respectively. The highest discrepancy was shown by the results from the visual observation during vanishing interfacial tension test and the lowest discrepancy was shown by the results from the swelling test. The vanishing interfacial tension test was found to be the fastest method for predicting the MMP. The method also consumed a smaller amount of oil and gas samples for the experiment. The simultaneous method proposed in this study is considered as more proper and exhibits a valuable method for predicting the MMP. This technique has never been found to be performed by previous researchers and accordingly it becomes the strong point of this study to contribute to the global research in the area of MMP determination.

1 Introduction

The Minimum Miscibility Pressure (MMP) is essential for CO₂ injection. The MMP can be determined either by laboratory experiments or numerical studies. Several researchers have introduced experiments methods for predicting the MMP such as Yellig and Metcalfe (1980), Christiansen and Haines (1987), Wang (1986), Hagen and Kossack (1986), Rao (1997), Tsau *et al.* (2010), Abdurrahman *et al.* (2015), Alomair *et al.* (2015), and Rahimi *et al.* (2017). Some other methods have also been introduced by Cronquist (1978), Johnson and Pollin (1981), Sebastian *et al.* (1985), Glaso (1985), Ahmed (2000), and Stalkup and Yuan (2005). However, each individual method has distinctive disadvantages in yielding the accurate values discussed by Danesh (1998), Johns and Orr (1996), Ayirala and Rao (2006), and Tsau *et al.* (2010). Several researchers have tried simultaneous method in order to reduce the uncertainties including Thomas *et al.* (1994), Elsharkawy *et al.* (1992), Ayirala and Rao (2006), Tsau *et al.* (2010),

and Abdurrahman *et al.* (2015). In their study, they compared the results using two or three methods to yield the more reliable MMP. Nevertheless, none of the mentioned researchers have compared the results of using more than three methods.

In this study, we propose a new approach to produce the MMP with high confidence level and less doubtful results. We use various methods including slim tube test, vanishing interfacial tension test, swelling test, visual observation through swelling and vanishing interfacial tests, and simulations in order to obtain the MMP. Our approach is to simultaneously plot results of slim tube test *vs.* swelling test, VIT test *vs.* swelling test, and slim tube test *vs.* VIT test in the same graph. In the analysis, we include results of visual observation and simulations to obtain more reasonable MMP value.

2 Preparation and procedures

Various stages are intentionally prepared to yield appropriate results of either slim tube test, swelling test, vanishing

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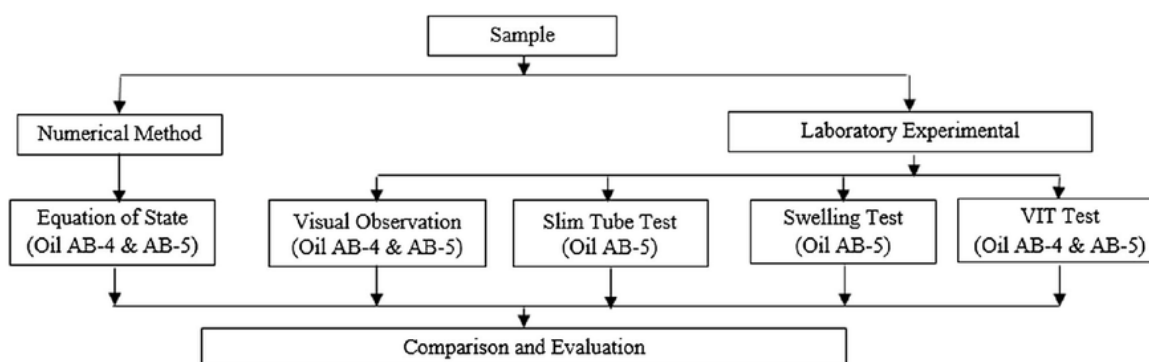


Fig. 1. The procedure of study.

interfacial test, visual observation, and simulation. Afterwards, the entire results are compared to each other as a means to examine any discrepancy among the results. Figure 1 exhibits the flowchart of our research methodology, while the following explanations describe each experiment stage conducted in the current study.

2.1 Light oil composition and CO₂ quality

Two types of crude oil are used in this study. The crude oil samples are taken from Layer AB-4 and AB-5 within Air Benakat Formation of South Sumatra Basin located in Jambi Province, Indonesia. The composition and other properties of the oil samples are shown in Tables 1, S1a, and S1b. The CO₂ gas used in this study has 99.99% of purity.

2.2 Experimental apparatus and procedures

2.2.1 Slim-tube test

The procedure for the experiments generally consists of three major stages including preparation, experiment, and cleaning stages. The stages applied for the slim tube test as well as the other tests. The preparation stage for the slim tube test includes leak testing, slim tube saturation using the sample of up to 2.0 PV, Back-Pressure Regulator (BPR) setting at the desired pressure, and air bath temperature system setting at the reservoir condition. The experimental stage involves CO₂ injection at the rate of 0.2 cc/min until it reaches 1.2 PV, effluent collection in the measuring cylinder and oil volume measurement. At the same time, the change in oil color is observed in the visual cell for estimating the condition of miscibility then the oil recovery is calculated for each pressure and the results are plotted. The cleaning stage involves oil sample cleaning in the slim tube using toluene and then nitrogen. The miscibility is estimated at the break-over point in the plot of recovery factor *vs.* pressure as suggested by Yellig and Metcalfe (1980). The experimental diagram of the slim tube test is shown in Figure S1. The description and specification of the slim tube is shown in Table S2.

2.2.2 Swelling test

The main apparatus used for the swelling test in the present study consists of a high-pressure cell made of sapphire glass. To fill-up the cell by CO₂ we use precision pump namely ISCO Pump 250DM. A heater is used to control the temperature of the air bath system. To help control the CO₂ liquid state before it is injected into the cell we use a cooler. To obtain images and to record the course of the experiment we use a simple camera located outside of the air bath system. A stirring bar located inside the cell is used to mix the CO₂ and oil until it reaches its equilibrium condition. A rare magnet located within a slot outside the cell is used to control the movement of the bar. Other standard auxiliary equipment for measuring pressure and temperature are also included in the experimental system. Our swelling test experimental diagram is shown in Figure 2.

2.2.3 Vanishing interfacial test

The experimental diagram of the vanishing interfacial test is shown in Figure S2. Two syringe pumps from ISCO Company is used for water and CO₂ injections and a goniometer apparatus from Rame-Hart Instrument Co. combined with a visual cell is used for this experiment. A high-pressure and high-temperature visual cell is equipped to measure the Interfacial Tension (IFT) in reservoir condition. The cell diameter is 30 mm, its height is 60 mm, and its thickness is 16 mm. The maximum operating pressure and temperature of the visual cell are 3000 psi and 300 °C, respectively. The needle, which has Outside Diameter (OD) of 0.91 mm and length of 50 mm and made from stainless steel is used. A pair of face-to-face sapphire-glass window is equipped within the visual cell. The glass windows with the thickness of 10 mm and the diameter of 30 mm is attached to the visual cell. A certain volume of dead-oil is mounted on the stainless-steel piston-chamber with 0–4000 psi maximum operating pressure. A metering valve and a check valve are applied to ensure the constant oil flow rate and to prevent the flow-back within the cell. The temperature is measured with a calibrated thermocouple located inside the cell. Afterwards, the pressure of the system is measured

Table 1. Sample properties (Abdurrahman et al., 2015).

Properties	AB-4	AB-5
API Gravity	20	41.38
Reservoir temperature (T_r) [°C]	60	65
Reservoir pressure (p_r) [psi]	786	1134
Bubble point pressure (p_b) [psi]	740	1116
Viscosity [cp]	4.6	0.21

through a pressure indicator. All apparatus is connected by using stainless steel tubing lines.

Before initiating the measurement, all lines and the apparatus is cleaned by using toluene, dried by using nitrogen, and vacuumed. The pressure inside the cell is conditioned by injecting some CO₂ into the cell. Then, the temperature condition is maintained constant by installing the heater. A sequential experiment is run with a serial condition of pressure that ranges from 700 to 2500 psi and temperature that ranges from 60 °C to 66 °C. After that, the pressure and temperature inside the cell are constantly maintained according to the desired condition which usually takes about 20–30 min. The water with a specific rate of 0.1 cc/min is pumped into the chamber and the piston pushes up the dead oil inside the chamber. The dead oil is flown from the chamber through the tubing line until it reaches the needle's tip. When the oil drop reaches the needle's tip, the drop hang and this condition is maintained at stable condition for a certain time by adjusting the metering valve. In this experiment, the stable condition of the drop should be maintained between 40 and 60 s. These time range has been suggested by previous researchers including Yang and Gu (2005) and Yang et al. (2015).

2.2.4 Visual observation

Visual observation during swelling test

Visual observation is performed through images captured as videos or pictures similar to the method conducted previously by Wang (1986). This method has also been performed by Abdurrahman et al. (2015). This method is aimed to observe visually the change in color of the oil as the pressure increases. The observation is done during the extraction-condensation stage when the swelling factor begins to decrease. The MMP should be obtained when the interface of the CO₂-rich phase and the CO₂ vapor disappears. According to Abdurrahman et al. (2015), this method is obviously not accurate and should be regarded only as an approximate method to estimate the MMP.

Visual observation during VIT test

Visual observation through videos or pictures during the vanishing interfacial test is used in determining the MMP in this study. This is aimed to observe the change in drop shape of the oil as the pressure increases. When the pressure in the view cell is increased, the CO₂ dissolves in the crude oil and the oil drop shape at the tip of the needle gradually changes. This phenomenon occurs until the oil drop disappears at the tip of the needle. The MMP is obtained when

the oil and the CO₂ become one phase or the oil drop disappears from the needle tip at some higher pressure. This phenomenon can be easily observed by visual means. Again, regardless this method is effective in recognizing when the miscibility occurs; it is obviously not accurate and should be regarded only as approximation.

2.2.5 Simulation

Zick (1986) discovered a combination between condensing and vaporizing gas drive mechanisms during miscibility process of CO₂ and crude oil. However, this phenomenon cannot be observed using ternary diagram. Therefore, according to Zick, various methods using numerical simulations have been proposed by Jaubert et al. (1998a, 1998b), and Jaubert et al. (2002). Jaubert et al. (1998a) pointed out their study on predicting the MMP using a slim tube simulator. The result showed excellent accuracies compared to 1D simulator. In addition, the compositional slim tube simulator was about 18–80 times faster compared to 1D simulator. Jaubert et al. (1998a) devoted their study on using real petroleum fluid model. They mentioned that one cell simulator has some limitations for estimating the MMP. Due to the time consuming and very expensive experiments for determining the MMP, Jaubert et al. (2002) conducted swelling and multiple contact tests in their study. They concluded that the two tests are faster and cheaper for predicting the MMP.

In these days, numerical simulators offer several options for predicting the MMP. This paper uses CMG simulator of which it provides options in WinProp that can be utilized to calculate the MMP. The Multiple-Contact Miscibility (MCM) option or the First-Contact Miscibility (FCM) pressure for a given oil and solvent at a particular temperature or the Minimum Miscibility Enrichment (MME) level that is required for the multiple- or single-contact miscibility at given temperature, pressure, oil composition, primary and make up gas composition are available in the program. The C7+ characterization has to be made since the splitting of the oil compositional data of the samples is not possible while the simulator requires components to be defined until C35. The MMP can then be determined for a given solvent composition by entering a range of pressure to be tested. The program reports the MMP if it is found and the mechanism by which the miscibility occurs is achieved. It could be vaporizing or condensing drive mechanisms.

For the MMP calculation in the present study, the pressure increment is divided into 10 steps. The calculation begins with the lowest pressure of 500 psi and terminates at the maximum pressure of 2500 psi. The results including the ternary diagrams are collected for each pressure step of which is used to specify the pressure range and values corresponding to the MMP. The required data for the simulation includes temperatures of 60 °C and 66 °C, pressures ranging from 500 psi to 2500 psi, oil composition, and the primary gas composition, i.e. the CO₂ with the purity of 99.99%. The equation of state used in this work is Peng–Robinson EOS. The viscosity model is that of Jossi–Stiel–Thodos with the aqueous phase salinity (or NaCl) concentration equals to zero. The simulator version is CMG/WinProp 2017.

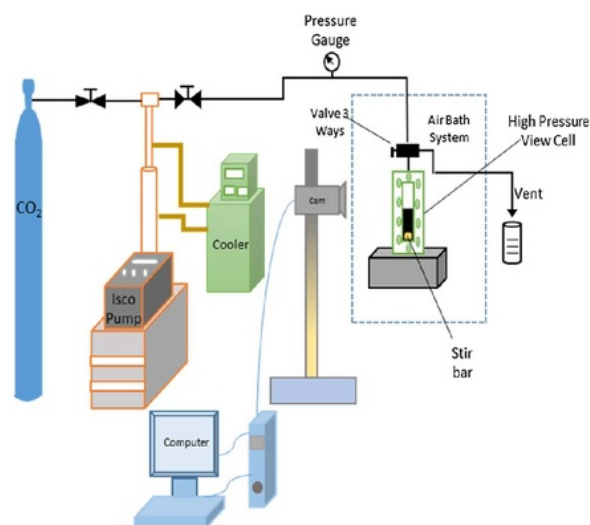


Fig. 2. The diagram of swelling test experiment (Abdurrahman et al., 2015).

3 Results

3.1 Estimating MMP by slim-tube test

The slim tube test experiment uses Crude Oil AB-5 for two reservoir temperature conditions of 60 °C and 66 °C. The slim tube experiment results for both temperatures are shown in Figure S3. The MMP is determined by using the break-over point technique as suggested by Yellig and Metcalfe (1980). The results from this slim tube experiment show that the miscibility occurs at 1540 psi and 1700 psi for the two temperature conditions of 60 °C and 66 °C, respectively.

3.2 Estimating MMP by plots of swelling factor vs. pressure

The swelling test experiment offers a new technique for estimating the MMP graphically by plotting the resulted swelling factor as a function of pressure. Tsau et al. (2010) suggested in their experiment on how to predict the MMP based on data resulted from a swelling test. The approach involves the determination of the MMP by recognizing the intersection between the extraction-condensation line and the condensation line.

Figure S4 shows that the intersection between the condensation-extraction line and the extraction line that occurs at the pressure of 1600 psi and 1700 psi. As a result, for the temperature of 60 °C, the MMP can be estimated as 1600 psi and for the temperature 66 °C, the MMP is obtained as 1700 psi. Due to some technical limitations, this method can only be applied to Crude Oil AB-5.

3.3 Estimating MMP by plots of IFT vs. pressure

An experimental study performed by Yang and Gu (2005) explained that during the diffusion process the light and

moderate components are rapidly extracted from the oil drop causing the CO₂ to be oil-rich. This phenomenon leads to the decrease of the Interfacial Tension (IFT) between the oil and the CO₂. However, when the pressure increases and reaches the near-miscibility condition the heavy component remains in the crude oil. At this condition, the oil drop begins to shrink and the IFT reduces quite slowly. Based on this explanation, in the present study two regions are recognized during the vanishing interfacial test. The first is referred to as Region A representing the diffusion stage and the second is referred to as Region B representing the shrinkage stage. In this regard, the MMP is determined by linear extrapolation of the diffusion line versus pressure data to zero value of IFT. A linear regression analysis for estimating the MMP of Crude Oil AB-5 at temperatures of 60 °C and 66 °C results in the equations below:

$$\text{IFT} = -0.0262 \times P + 42.22, \quad (1)$$

$$\text{IFT} = -0.0226 \times P + 40.17. \quad (2)$$

The first equation is for estimating the MMP at 60 °C with the correlation coefficient is found to be $R^2 = 99.99\%$. The second equation is for estimating the MMP at 66 °C with the correlation coefficient is found to be $R^2 = 99.99\%$. According to the value of R^2 for these equations, it is believed that the estimated MMP is considerably acceptable. Nevertheless, these equations can only be applied to a pressure range between 700 psi and 1500 psi for the temperature of 60 °C and between 700 psi to 1550 psi for the temperature of 66 °C. Above these two-pressure ranges the equation may not be applicable due to the occurrence of different phenomena.

Similarly, a linear regression analysis for estimating the MMP of Crude Oil AB-4 at temperatures of 60 °C and 66 °C results in the equations below:

$$\text{IFT} = -0.0255 \times P + 48.92, \quad (3)$$

$$\text{IFT} = -0.0258 \times P + 53.44. \quad (4)$$

The first equation is for estimating the MMP at 60 °C with the correlation coefficient is found to be $R^2 = 98.7\%$. The second equation is for estimating the MMP at 66 °C with the correlation coefficient is found to be $R^2 = 99.1\%$. According to the value of R^2 for these equations, it is also believed that the estimated MMP is considerably acceptable. Again, because of the occurrence of different phenomena at other pressure values, these equations can only be applied to a pressure range between 700 psi and 1800 psi for the temperature of 60 °C and 700 and 1900 psi for the temperature of 66 °C.

The MMP estimates under elevated pressure and temperature for Crude Oil AB-5 are shown in Figure S5 while the MMP estimates for Crude Oil AB-4 are shown in Figure S6. Using Equations (1) and (2) at the IFT value equals to zero the interfacial tension shows that the miscibility in Crude Oil AB-5 occurs at 1611 psi and 1777 psi for the

temperatures of 60 °C and 66 °C, respectively. It can also be seen that the MMP increases as the temperature increases. Increasing the temperature from 60 °C to 66 °C causes the increase in the MMP of about 166 psi or 27.7 psi/°C. Similarly, using Equations (3) and (4) at the IFT value equals to zero the interfacial tension shows that the miscibility in Crude Oil AB-4 occurs at 1918 psi and 2072 psi for the temperatures of 60 °C and 66 °C, respectively. The MMP also increases as the temperature increases. The increase in temperature from 60 °C to 66 °C causes the increase in the MMP of about 154 psi or 25.7 psi/°C. These results are reasonably consistent with those of Hemmati-Sarapardeh et al. (2013). In their study, the increase of the MMP is about 22.6 psi/°C. At higher temperature, the CO₂ solubility in the crude oil is lower, which results in a higher MMP.

3.4 Estimating MMP by visual observations during swelling test and vanishing interfacial test

3.4.1 Visual observation during swelling test

The MMP may be estimated by visual observation during the swelling tests as suggested by Wang (1986). In the present study, the observation is focused on the occurrence when the swelling factor begins to decrease which happens in the extraction-condensation stage. It should be noted here that the MMP estimate through visual observation is certainly subjective and may not reflect the correct MMP. The timing when the extraction-condensation and the extraction stages occur in the cell should also be determined carefully. Relating to the means the MMP is defined, the MMP is estimated when the interface of the CO₂-rich phase and the CO₂ vapor disappears. Figures S7 and S8 depict the phenomenon during the swelling test for Crude Oil AB-5. The oil color changes slightly as the pressure increases. The more notable oil color change occurs when the swelling factor starts to decrease suggesting that the miscibility of the CO₂ and the oil has been achieved. As mentioned by Huang et al. (1989) and Wang (1986), the phenomenon when the oil color starts to change from its original color as the pressure increases is known as the transition zone. While the pressure keeps increasing at this stage, the CO₂ and the oil dissolve each other and eventually become one phase. Then, the color of the oil looks brighter. In this experiment, the oil color starts to change at the pressure of 1600 psi and 1700 psi for the temperature of 60 °C and 66 °C, respectively.

In the extraction process, the pressure is higher than the MMP and the oil color changes to even much brighter as can be seen in Figure S9. This phenomenon results from a large number of moderate components of the oil that has been extracted leaving only the heavier components to remain at the bottom of the cell. The heaviest component subsequently precipitates in the form of black asphaltic flakes as it was also observed by Wang (1986). Assuming the yellow color observed within the cell represents the moderate components, this finding reveals clear evidences that the CO₂ extracts only the intermediate components of the oil. Similar observation results were also obtained by previous investigators. In their reports, it was mentioned that the CO₂ can extract only the oil components of C₅ to

C₃₀ (Stalkup, 1984). Photographic sketches illustrating the process of miscibility development were demonstrated by Wang (1986) when the oil shrinks to its minimum volume.

3.4.2 Visual observation during VIT test

Wang (1986) suggested that the MMP can be estimated visually during a swelling test experiment. The method has also been done by Abdurrahman et al. (2015) to predict the MMP in their experiments. In the present work, the MMP is also proposed to be predicted by visual observation. Figure S10 depicts the phenomena in Crude Oil AB-5 during vanishing interfacial test at the temperature of 60 °C. Clearly, at 1700 psi, the oil drop shape cannot be recognized as can be seen in the figure. Figure S11 depicts the same phenomena during the vanishing interfacial test for Crude Oil AB-5 at the temperature of 66 °C. The oil drop shape slightly changes as the pressure increases. In this experiment, the oil drop shape starts to change its shape to an irregular form when the pressure is higher than 1650 psi. At the pressure of 1800 psi, the oil drop shape cannot be recognized clearly as can be seen in the figure.

Figure S12 depicts the phenomena during the vanishing interfacial test at the temperature of 60 °C for Crude Oil AB-4. The oil drop slightly changes as the pressure increases. It is clearly seen during the experiment that the oil drop shape does not change to irregular form until the pressure reaches 2600 psi. The IFT between oil and CO₂ at this pressure is 0.91 dyne/cm. This value can be categorized as ultra-low IFT. Figure S13 depicts similar phenomena for Crude Oil AB-4 during the vanishing interfacial test at the temperature of 66 °C. It is also clearly seen from the figure that the oil drop shape does not change to any irregular form until the pressure is increased to 2600 psi. This is the highest pressure possible during the experiment. Any changes above this pressure is not possible due to some technical reasons. At the pressure of 2600 psi, the drop shape is still recognized as regular and the interfacial tension between the oil and CO₂ at this pressure is found to be 2.41 dyne/cm.

3.5 Determining MMP by simulations

Our simulation results using Peng–Robinson EOS calculated the MMP for Crude Oil AB-5 as 1670 psi and 1790 psi at 60 °C and 66 °C, respectively. Similarly, for Crude Oil AB-4, the MMP was found to be 2030 psi and 2240 psi at 60 °C and 66 °C, respectively. The cell-to-cell method is used in estimating the miscibility by detecting the pressure at which the tie line reaches the critical point. The simulation method is much faster than the experiment. It also does not require much input data. In this work, the MMP calculation is done without any tuning in predicting the phase behavior as suggested by Danesh (1998). The critical properties of the hydrocarbon and non-hydrocarbon components are defined in the simulator as shown in Table S3. The binary interaction coefficients between the hydrocarbon and non-hydrocarbon components are shown in Table S4 and Table S5.

4 Discussion

4.1 Comparing MMP estimations between slim-tube vs. pressure and swelling factor vs. pressure

In this analysis, the MMP is determined graphically from the results of the swelling test by plotting the swelling factor as a function of pressure. This can only be done for Crude Oil AB-5 because of the limited data from the slim tube test. As suggested by Tsau et al. (2010), the MMP can be obtained when the straight-line curves of the extraction-condensation stage and the extraction stage intersects each other. Therefore, the two curves representing the two stages are important to estimate the occurrence of miscibility and accordingly the MMP cannot be estimated with high-level of certainty if the straight lines cannot be well developed from the experimental data. In the condensation-extraction stage that is also called near-miscibility condition, the light-to-moderate components vaporize quite fast. Meanwhile, due to the already-reduced amount of the components, less moderate components vaporize in the extraction stage. The swelling factor decreases in both stages because CO₂ has extracted the light-to-moderate components. The intersection between the extraction-condensation and extraction straight lines is therefore crucial to construct in order to ensure the correct miscibility pressure. The solubility of CO₂ in oil increases as the pressure increases during the condensation stage and so the swelling factor. At some point, the oil is rich with the CO₂ and at the same time the oil reaches its maximum swelling factor. It is clearly shown in Figure S4 that the swelling factor reaches its maximum value of about 1.3 at 1400 psi. The miscibility, however, has not yet occurred. After the oil is fully saturated by CO₂, the extraction-condensation stage begins and few moderate components of the oil move into the CO₂ phase as indicated by the decrease in swelling factor. The extraction stage occurs as the pressure increases further where the CO₂ vaporizes and more moderate components leave the oil phase causing the swelling factor to decrease continuously but at different rate. As a result, for the temperature of 60 °C, the MMP is determined as 1600 psi (see Fig. S4). Using the same procedure, the results for the other temperature of 66 °C is also shown in Figure S4. The MMP for this case is obtained as 1700 psi. One thing that is important to note here is the effect of CO₂ solubility on the swelling factor. At higher pressure, the CO₂ solubility is also higher making its effect on the swelling factor is more significant. Therefore, the swelling factor of 1.4 at 66 °C and 1600 psi that is higher than that of 1.3 at 60 °C and 1400 psi in these experiments is mainly due to the effect of pressure which is more dominant than temperature.

It is clearly understood from Figure S4 that the MMP cannot be determined if the extraction stage does not occur so that the intersection between the straight-lines of the extraction-condensation stage and the extraction stage cannot be identified. Because the extraction stage is quite faster than the rate of swelling after the miscibility occurs, the extraction causes the swelling factor to decrease rapidly. This phenomenon was also reported by previous investigators such as Tsau et al. (2010) and Harmon and Grigg (1988).

Regardless the dominant effect of pressure, the temperature in fact plays an important role in the extraction-condensation stage as well as in the extraction stage that follows. Because the solubility of CO₂ in oil is low at higher temperatures, the extraction of the oil components is also low. Thus, during the CO₂ injection process at the higher temperature of 66 °C, the CO₂ dissolves only slightly in the oil as indicated in Figure S4 causing low concentration of the hydrocarbon that can be extracted. As a result, the oil shrinkage is also low during the extraction-condensation stage and the oil volume returns to its initial condition as indicated by the swelling factor of unity. When the injection is conducted at the lower temperature of 60 °C, a different phenomenon occurs where more CO₂ dissolves into the oil and the oil shrinkage is quite high as indicated in Figure S4. Then, because more oil components are extracted during the extraction-condensation stage, the swelling factor decreases to a value of less than 1.0. However, when the temperature increases, the MMP also increases. In the present study, the increase in temperature of 6 °C leads to the increase of the MMP by 100 psi or about 16.7 psi/°C. This result is very much close to the result of the work by Elsharkawy et al. (1992). They reported that the increase of the MMP affected by the increase of temperature fell within the range of 18.10 psi/°C and 27.02 psi/°C. Figure S4 clearly show this effect of temperature on the MMP. At higher temperatures, the condensation-extraction and the extraction lines will be slightly flatter than the lines at lower temperatures. The logical reasoning for this phenomenon may be because at higher temperature the CO₂ extract less oil components and accordingly it requires higher pressure to achieve miscibility condition resulting in higher MMP.

Figure S14 displays combined plots comparing the results of the slim tube experiment and those of the swelling test each of which for the temperatures of 60 °C and 66 °C. Analyzing the plots graphically, the MMP resulted from the swelling test is obviously in good agreement with that from the slim tube experiment. In other words, the MMP obtained from the swelling test in the present study is considerably correct. This results therefore invalidates the doubting relationship previously noted by Harmon and Grigg (1988) between the MMP obtained from the slim tube experiment and that from the swelling test. The difference between the MMP obtained from the slim tube and that from the swelling test is about 3.9% for the temperature of 60 °C and basically zero for the temperature of 66 °C (see Table S6).

4.2 Comparing MMP estimations between swelling factor vs. vanishing interfacial test

In this analysis, the results for Crude Oil AB-5 are examined. Figure S15 shows combined plots comparing the results of the vanishing interfacial test and that of the swelling test at the temperatures of 60 °C and 66 °C, respectively. A graphical analysis on the plots clearly shown that the MMP resulted from the swelling test is also in good agreement with that of the vanishing interfacial test. As a result, the MMP obtained from the swelling test and that from the vanishing interfacial test in the present study

proposed to be considerably correct. As displayed in Table S7, the differences between the results of the swelling test and that of the vanishing interfacial test are about 0.7% and 4.3% for the temperature of 60 °C and 66 °C, respectively. It follows that the MMP obtained from the swelling test and that from the vanishing interfacial test at low temperatures are closer to each other than the same results at higher temperatures. In the meantime, the MMP obtained from vanishing interfacial test is slightly higher than that obtained from the swelling test. However, the difference is still reasonable as it is considerably a small figure.

Following the explanation provided by Yang and Gu (2005), two regions namely Region A for diffusion stage and Region B for shrinkage stage are recognized. In Region A the CO₂ diffuses into the crude oil causing the oil to swell and accordingly the Interfacial Tension (IFT) to decrease. In this study, the IFT in Region A is found to decrease from 24.5 dyne/cm to 2.93 dyne/cm at 60 °C and 24.9 dyne/cm to 3.4 dyne/cm at 66 °C. However, as the pressure continues to increase the oil drop is lacking of moderate component leaving heavy component as the main constituent of the oil drop. In that condition the oil volume decreases owing to the shrinkage of the oil drop. On the other hand, in Region B the remaining heavy component in the oil drop only causes the IFT to slowly decrease. In this region, the IFT decreases from 2.6 dyne/cm to 2.5 dyne/cm at 60 °C and 3.0 dyne/cm to 2.1 dyne/cm at 66 °C. This phenomenon is clearly shown in Figure S15. Regarding the MMP explanations according to the molecular effects, the logical reasoning may be expressed as follows. When the CO₂ injection pressure increases at Region A, more CO₂ molecules will diffuse into the oil. Thus, the oil density decreases rapidly. The higher the injection pressure, the denser the CO₂ causing its density to be higher. This condition minimizes the density difference between the CO₂ and the oil drop. Lower density difference means the operating intermolecular forces between the CO₂ and the oil will be close at Region B. The interface between the CO₂ and the oil disappears when the operating intermolecular force between the two phases is in balanced condition. It is also believed that near-miscibility occurs at the intersecting point between Region A and B lines in the plot of the IFT *vs.* pressure. Prior to the near-miscibility region the IFT decreases more rapidly as the pressure increases. In contrast, after the near-miscibility region (or shrinkage region) the IFT continue but slowly decreases as the pressure increases. This is probably because of the domination of the heavy component.

It follows from the above that the existence of the intersecting lines of the extraction-condensation and the extraction stages is crucial in estimating the MMP through swelling test. During the swelling test, three regions namely condensation, condensation-extraction, and extraction occur and can be recognized easily. These regions do not exist and cannot be recognized during the vanishing interfacial test. The logical reasoning may be expressed as follows. When the swelling test is conducted, the oil volume is as much as 2.1 mL and it causes more CO₂ to dissolve into the oil. In that process, it is easy to recognize the three regions through the view cell. However, when a vanishing

interfacial test is conducted the oil surrounded by the CO₂ is too small averaging only 3–8 µL. Because of the small oil volume, the process is not able to depict the three regions such as the process occurs during swelling test. However, from the similarity of the curve trend and the slope changes between the swelling test and the vanishing interfacial test during the extraction process it is believed that at the pressure above the MMP the heavy component is dominating the oil composition. Figure S4 as well as Figures S5 to S6 may be useful to describe such phenomenon.

It is unfortunate that due to some technical reasons the swelling test and the slim tube test cannot be performed for Crude Oil AB-4. Therefore, the similar analysis to the results for Crude Oil AB-5 cannot be done for Crude Oil AB-4. However, as the composition may affect considerably the MMP as explained above, the higher molecular weight of the heptane-plus in Crude Oil AB-4 compared to Crude Oil AB-5 may be responsible for the higher MMP of Crude Oil AB-4 in the IFT experiment at both temperatures of 60 °C and 66 °C. To be precise, different composition between the two oil samples results in different MMP. In this case, the higher content of heavy component in Crude Oil AB-4 results in the higher MMP. Line B or shrinkage line of the IFT results proves the heavy component richness of Crude Oil AB-4. Also, the IFT still exist even at high pressures. Hence, the MMP in Crude Oil AB-4 is logically higher than that of Crude Oil AB-5. Table S8 shows the comparison of the MMP for the two oil samples based on the VIT test results.

4.3 Comparing MMP estimations by slim tube vs. VIT test

Because of the slim tube and VIT tests results availability, further analysis can be done for Crude Oil AB-5. Figure S16 shows combine plots comparing the results of the slim tube and VIT tests at 60 °C and 66 °C, respectively. The MMP resulted from the VIT test is in good agreement with that obtained from the slim tube test. It then follows that the MMP obtained from the VIT test is considered satisfactorily correct. By plotting the slim tube and the VIT tests results in the same graph, the uncertain and doubtful MMP from the VIT result can be diminished. The plot also provides enhancement to the MMP estimation. Table S9 shows the results of the MMP as well as their differences between the two tests. As shown in the table, the discrepancies between the two methods are 4.5% at 66 °C and 4.6% at 66 °C, respectively. In other words, the effect of temperature is not significant.

4.4 Comparing MMP estimations by experiments vs. simulation

The slight disagreement between the results of experimental and simulation methods is most likely caused by the specific property of the oil sample used in each method. The slim tube test, the vanishing interfacial test and the swelling test use dead oil samples while the simulation uses live oil samples. The gas composition in the live oil sample such as methane and nitrogen causes the MMP slightly higher

(Dong et al., 2000). Table S10 shows the differences between the results of the swelling test and the simulation for Crude Oil AB-5 are about 4.2% and 5.0% at the temperature of 60 °C and 66 °C, respectively. Meanwhile, the differences between the results of the vanishing interfacial test and that of the simulation are about 3.5% and 0.7% at the temperature of 60 °C and 66 °C, respectively. Then, the differences between the results of the slim tube test and that of simulation are about 7.8% and 5.0% at the temperature of 60 °C and 66 °C, respectively. It then follows that all the experimental methods including the swelling test, the vanishing interfacial test, and the slim tube test provide satisfactory estimates of the MMP. It can also be seen in the table that the MMP estimated by the VIT method has the closest value to the MMP from the EOS method. In contrast, the highest difference from EOS method is the results of the slim tube test. Furthermore, the difference of the MMP values obtained from swelling test to that of the EOS is consistent at both temperatures. As a conclusion, the MMP at a specific temperature resulted from the methods used in the present study does not show a single or exactly the same value. There is always a discrepancy among the results no matter how small it is.

Generally, the MMP data obtained from the use of EOS is higher than those obtain from experimental methods including the VIT test, the swelling test, and the slim tube test particularly for Crude Oil AB-4. Shown in Table S11, the difference between the results of the vanishing interfacial test and the simulation is about 5.5% at the temperature of 60 °C and 7.5% at 66 °C. Clearly the difference of the MMP using EOS is higher for Crude Oil AB-4 than that of Crude Oil AB-5. It may provide further information and possible analysis if there are some data obtained from slim tube and swelling tests for Crude Oil AB-4. Accordingly, there may some other conclusions that can be drawn.

5 Conclusion

Drawing from the results of the present study, the following are summarized conclusions.

1. Very few investigators used simultaneous methods in predicting the MMP.
2. Analysis using data plotting from simultaneous methods has never been examined in detail previously.
3. The use of simultaneous methods is able to reduce uncertainties and doubts of the resulted MMP.
4. The MMP obtained from the slim tube test has been used as the standard result or baseline in the present study.
5. The visual observation either during the swelling test or interfacial tension test is worthy for recognizing the timing of the miscibility to occur during experiments.
6. The interfacial tension test is the most effective method in utilizing oil samples and gas for the experiment. Less time consumption and small amount of oil and gas to utilize are the main advantages of using this method regardless the analysis that shows slightly higher discrepancies than that of the slim tube test.

7. Despite the closeness of the results, each method has shown results that are in fact different to each other. However, in general, all the methods can be properly used for predicting the MMP.

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Supplementary Material

Supplementary material is available at <http://ogst.ifpenergiesnouvelles.fr/10.2516/ogst/2019028/olm>.

References

- Abdurrahman M., Permadi A.K., Bae W.S. (2015) An improved method for estimating minimum miscibility pressure through condensation – extraction process under swelling tests, *J. Pet. Sci. Eng.* **131**, 165–171. <https://doi.org/10.1016/j.petrol.2015.04.033>.
- Ahmed T. (2000) Minimum Miscibility Pressure from EOS, *Petroleum Society of Canada – Canadian International Petroleum Conference*, 4–8 June, Calgary, Alberta. <https://doi.org/10.2118/2000-001>.
- Alomair O., Malallah A., Elsharkawy A., Iqbal M. (2015) Predicting CO₂ Minimum Miscibility Pressure (MMP) using Alternating Conditional Expectation (ACE) algorithm, *Oil Gas Sci. Technol. - Rev. IFP Energies nouvelles* **70**, 6, 967–982. <https://doi.org/10.2516/ogst/2012097>.
- Ayrala S.C., Rao D.N. (2006) Comparative Evaluation of a New MMP Determination Technique, *Society of Petroleum Engineers – SPE/DOE Symposium on Improved Oil Recovery*, 22–26 April, Tulsa, Oklahoma, USA. <https://doi.org/10.2118/99606-MS>.
- Christiansen R.L., Haines H.K. (1987) Rapid measurement of minimum miscibility pressure with the rising-bubble apparatus, *Soc. Pet. Eng. - SPE Reserv. Eng.* **2**, 4, 523–527. <https://doi.org/10.2118/13114-PA>.
- CMG Software (2014) *WinProp User's Guide*, Computer Modelling Group, Calgary, Alberta, Canada.
- Cronquist C. (1978) Carbon dioxide dynamic miscibility with light reservoir oils, *US Doe Annual Symposium*, Tulsa.
- Danesh A. (1998) *PVT and phase behaviour of petroleum reservoir fluids*.
- Dong M., Huang S., Srivastava R. (2000) Effect of solution gas in oil on CO₂ minimum miscibility pressure, *J. Can. Pet. Technol.* **39**, 11. <https://doi.org/10.2118/00-11-05>.
- Elsharkawy A.M., Poettmann F.H., Christiansen R.L. (1992) Measuring minimum miscibility pressure: slim-tube or rising-bubble method? *Soc. Pet. Eng.* <https://doi.org/10.2118/24114-MS>.
- Glaso O. (1991) Generalized minimum miscibility pressure correlation, *Soc. Pet. Eng.* **25**, 6. <https://doi.org/10.2118/12893-PA>.

- 1 Hagen S., Kossack C.A. (1986) Determination of minimum
2 miscibility pressure using a high-pressure visual sapphire cell,
3 *Society of Petroleum Engineers – SPE Enhanced Oil Recovery*
4 *Symposium*, 20–23 April, Tulsa, Oklahoma. <https://doi.org/10.2118/14927-MS>.
5
- 6 Harmon R.A., Grigg R.B. (1988) Vapor-density measurement
7 for estimating minimum miscibility pressure, *Society of*
8 *Petroleum Engineers – SPE Reservoir Engineering*, **3**, 4.
9 <https://doi.org/10.2118/15403-PA>.
- 10 Hemmati-Sarapardeh A., Ayatollahi S., Ghazanfari M.-H.,
11 Masihi M. (2013) Experimental determination of interfacial
12 tension and miscibility of the CO₂ – crude oil system;
13 Q6 temperature, pressure, and composition effects, *J. Chem.*
14 *Eng. Data* **61**, 61–69. <https://doi.org/10.1021/je400811h>.
15
- 16 Huang S.S., de Wit P., Jha K.N. (1989) A laboratory miscible
17 displacement study for the recovery of Saskatchewan's crude
18 oil *Petroleum Society of Canada - Petroleum Conference of*
19 *The South Saskatchewan Section*, 25–27 September, Regina.
20 <https://doi.org/10.2118/SS-89-03>.
- 21 Jaubert J.-N., Arras L., Neau E., Avasulle L. (1998a) Properly
22 defining the classical vaporizing and condensing mechanisms
23 when a gas is injected into a crude oil, *Ind. Eng. Chem. Res*
24 **37**, 1, 4860–4869. <https://doi.org/10.1021/ie9803016>.
25
- 26 Jaubert J.-N., Wolff L., Neau E., Avasulle L. (1998b) A very
27 simple multiple mixing cell calculation to compute the
28 minimum miscibility pressure whatever the displacement
29 mechanism, *Ind. Eng. Chem. Res* **37**, 4854–4859,
30 <https://doi.org/10.1021/ie980348r>.
31
- 32 Jaubert J.-N., Avasulle L., Pierre C. (2002) Is it still necessary to
33 measure the minimum miscibility pressure? *Ind. Eng. Chem.*
34 *Res.* **41**, 303–310. <https://doi.org/10.1021/ie010485f>.
35
- 36 Johnson J.P., Pollin J.S. (1981) Measurement and correlation of
37 CO₂ miscibility pressures, *Society of Petroleum Engineers*.
38 <https://doi.org/10.2118/9790-MS>.
39
- 40 Rahimi V., Bidarigh M., Bahrami P. (2017) Experimental study
41 and performance investigation of miscible water-alternating-
42 Q10 CO₂ flooding for enhancing oil recovery in the Sarvak
43 formation, *Oil Gas Sci. Technol. - Rev. IFP Energies*
44 *nouvelles* **72**, 6, 35, <https://doi.org/10.2516/ogst/2017030>.
45
- 46 Rao D.N. (1997) A new technique of vanishing interfacial
47 tension for miscibility determination, *J. Fluid Phase Equilibria*
48 **139**, 1–2, 311–324. [https://doi.org/10.1016/S0378-3812\(97\)](https://doi.org/10.1016/S0378-3812(97)00180-5)
49 [00180-5](https://doi.org/10.1016/S0378-3812(97)00180-5).
- 50 Sebastian H.M., Wenger R.S., Renner T.A. (1985) Correlation of
51 minimum miscibility pressure for impure CO₂ streams, *J. Pet.*
52 *Technol.* **37**, 11, <https://doi.org/10.2118/12648-PA>.
53
- 54 Stalkup F.I. (1984) Miscible Displacement (SPE Monograph
55 Series), *Society of Petroleum Engineers of AIME*, Dallas –
56 New York.
- 57 Stalkup F., Yuan H. (2005) Effect of EOS characterization on
58 predicted miscibility pressure, *Society of Petroleum Engi-*
59 *neers – SPE Annual Technical Conference and Exhibition*, 9–
60 12 October, Dallas, Texas.
- 61 Thomas F.B., Zhou X.L., Bennion D.B., Bennion D.W. (1994) A
62 comparative study of RBA, P-x, m, contact and slim tube
63 results, *J. Can. Pet. Technol.* **33**, 2, [https://doi.org/10.2118/](https://doi.org/10.2118/94-02-02)
64 [94-02-02](https://doi.org/10.2118/94-02-02).
65
- 66 Tsau J.S., Bui L.H., Willhite G.P. (2010) Swelling/extraction
67 test of a small sample size for phase behavior study *Society of*
68 *Petroleum Engineers – SPE Improved Oil Recovery Sympo-*
69 *sium*, 24–28 April, Tulsa, Oklahoma, USA. <https://doi.org/10.2118/129728-MS>.
70
- 71 Wang G.C. (1986) A study of crude oil composition during CO₂
72 extraction process, *Society of Petroleum Engineers*.
73 <https://doi.org/10.2118/15085-MS>.
74
- 75 Yang D., Gu Y. (2005) Interfacial interactions between crude oil
76 and CO₂ under reservoir conditions, *Pet. Sci. Technol.*
77 (November 2014), 37–41, [https://doi.org/10.1081/LFT-](https://doi.org/10.1081/LFT-200035536)
78 [200035536](https://doi.org/10.1081/LFT-200035536).
79
- 80 Yang Z., Liu X., Hua Z., Ling Y., Li M., Lin M., Dong Z. (2015)
81 Interfacial tension of CO₂ and crude oils under high pressure
82 and temperature, *Colloids Surf. A Physicochem. Eng. Aspects*
83 **482**, 611–616. <https://doi.org/10.1016/j.colsurfa.2015.05.058>.
84
- 85 Yellig W.F., Metcalfe R.S. (1980) Determination and prediction
86 of CO₂ minimum miscibility pressures, *J. Pet. Technol.* **32**, 1,
87 <https://doi.org/10.2118/7477-PA>.
88
- 89 Zick A.A. (1986) A combined condensing/vaporizing mechanism
90 displacement of oil by enriched gases, *Society of Petroleum*
91 *Engineers – SPE Annual Technical Conference and Exhibi-*
92 *tion*, 5–8 October, New Orleans, Louisiana. <https://doi.org/10.2118/15493-MS>.
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